Time-Dependent Creep Response of Magneto-Electro-Elastic Rotating Disc in Thermal and Humid Environmental Condition

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Abstract

The aim of this paper is to analyze the time-dependent stress redistribution of a rotating magneto-electro-elastic (MEE) disc. The disc is supposed to be placed in an axisymmetric temperature and moisture fields. Besides, the disc is under a centrifugal body force, an induced electric potential in addition to magnetic potential. Using equilibrium, electrostatic and magnetostatic equations, strain-displacement and stress-strain relations together with hygrothermal equations, a differential equation is obtained in which there are creep strains. Primarily, disregarding the creep strain, an analytical solution for the initial stresses, electromagnetic potentials and displacement is developed. Then, using Prandtl-Reuss relations, creep stress rates and electromagnetic potentials rates are obtained. Finally, the history of stresses, electric and magnetic potentials is obtained iteratively. In the numerical section, the influence of creep evolution, hygrothermal environmental condition, angular velocity and temperature- and moisture-dependency of elastic coefficients on the behavior of MEE disc is analyzed comprehensively. The results show that the effect of hygrothermal loading and angular velocity becomes less significant after creep evolution. Also, the results imply that analysis of the effect of temperature- and moisture- dependence after creep evolution must be considered in the design progress. Besides, to avoid cracking, increasing in the tensile hoop stress at the internal surface with increasing in hygrothermal loading must be considered in design progress.

Keywords: Rotating disc, Magneto-electro-elastic, Time-dependent creep, Hygrothermal loading
1. Introduction

Due to huge application of rotating disc in rotating machinery, they have been focused by many researchers. They have many industrial usages such as compressors, turbo generators, flywheels, gas turbine rotors, automotive braking systems, ship propellers and computer disc drives [1]. On the other hand, MEE composites that are a type of intelligent materials have been focused by many researchers. Due to the presence of magnetic and electric coupling effect, these materials allow an extra degree of freedom in the design of actuators, sensors, storage devices and transducers. Their requests can be found in turbine rotors, aerospace, magnetic storage elements and magnetic structural elements.

Since smart materials are mostly selected to work in presence of magnetic field or in high temperature and humid environments [2], several papers are presented in the literature for static hygrothermal analysis of them. Akbarzadeh and Chen [3] presented a solution for hygrothermal stress problem in functionally graded piezoelectric material (FGPM) cylinder and spheres. Analysis of the interaction of electric field, elastic deformation, thermal and moisture condition in hollow and solid piezoelectric cylinders was presented by Allam et al [4]. Saadatfar and Aghaie-Khafri [5] analyzed the static response of a functionally graded MEE (FGMEE) thick-walled sphere in thermal and humid condition using an analytical method. A long functionally graded material (FGM) cylindrical shell with FGPM sensor and actuators under magneto-thermo-electro-elastic loading was analyzed analytically by Saadatfar and Aghaie-Khafri [6]. Also, they [7] illustrated that the actuation and sensing authority of FGPM layers mostly affected by the grading-index of the FGPM. Then, Saadatfar and Aghaie-Khafri considered a FGM cylindrical shell integrated with FGPM layers subjected to magneto-thermo-electro-elastic [8, 9] hygro-thermo-electro-elastic [10] and hygro-thermo-magneto-electro-elastic [11] loadings. A closed-form solution for a piezoelectric functionally graded fiber-reinforced hollow cylinder in hygrothermal condition was derived by Zenkour [12]. The static analysis of MEE plate in hygrothermal environment
was presented by Vinyas and Kattimani [13] using the finite element method. Thermoelastic behavior of a rotating disc with variable thickness made of FGMEE was presented by Dai and Dai [14]. Also, several authors have tried to analyze the creep response of composite, FGM and smart discs. Using Sherby's law, the creep progress of an isotropic FGM rotating disk with thermal gradient was considered by Gupta et al. [15]. Creep behavior of FGM rotating disks with linearly varying thickness was investigated by Deepak [16]. Rattan et al. [17] tried to analyze the creep progress of an isotropic rotating disk made of particle reinforced FGM. Dharmal et al. [18] analyzed the steady-state stress redistribution in a FGM rotating disk with variable thickness. Gupta and Singh [19] made an attempt to present an analytical method to analyze the creep progress in non-FGM/FGM rotating disk with uniform and non-uniform thickness. The steady-state creep behavior of an isotropic rotating disk made of parabolically varying FGM in thermal environment is investigated by Bose and Rattan [20]. Loghman et al. [21] considered the creep response of FGPM rotating disc under magneto-electro-thermal loads using a semi-analytical method. They show that the history of electric potential can be used for condition monitoring of the smart disk without any need to destructive or non-destructive testing. A new analytical-numerical way to analyze creep evolution of rotating disk made of nonlinear piezoelectric polymer in thermal environmental condition was presented by Loghman and Azami [22]. They show that a significant electric potential redistribution due to stress redistribution has occurred during the lifetime of the disk.

Literature review reveals that creep analysis is vital for rotating disk. Also, smart materials are subjected to hygrothermal loading in some of their application. Moreover, they show considerable creep effects under severe environmental condition [23]. Therefore, to have advanced performance and reliability of intelligent structures, creep response must be investigated when MEE structures are used in hygrothermal environmental condition. However, the creep analysis has not been investigated for the MEE disc so far. So, the novelty of the present research is to investigate the time-dependent creep stress and electric and magnetic potentials redistributions during the lifetime of a MEE disc in steady-state hygrothermal
environment considering temperature and moisture dependency of elastic constants using analytical methods.

2. Basic formulation of the problem

Consider a uniform thickness MEE disc rotates about z axis with a constant speed as shown in Fig. 1. The disc is assumed to be subjected to hygrothermal field in addition to electro-magnetic potentials at inner and outer surfaces. Regarding symmetry and plane stress condition, nonzero components of temperature, moisture concentration, electric potential, magnetic potential and displacement are function of radius.

![Fig. 1 MEE rotating disc](image)

2.1 Formulation of the hygrothermal field

In an uncoupled hygrothermal analysis, the temperature distribution as well as moisture concentration distribution can be achieved independently [24]. The Fourier heat conduction equation and Fickian moisture diffusion equation without source of heat and moisture for a disc in axisymmetric steady-state condition are expressed as [25, 26]:

\[
\frac{1}{r} \frac{\partial}{\partial r} \left( rk^T \frac{\partial T}{\partial r} \right) = 0, \quad (1.a)
\]

\[
\frac{1}{r} \frac{\partial}{\partial r} \left( rk^c \frac{\partial M}{\partial r} \right) = 0, \quad (1.b)
\]

Integrating Eqs. (1) twice gives:
\[ T(r) = W_1 \ln(r) - W_2, \]
\[ M(r) = S_1 \ln(r) - S_2. \]

In this research, moisture concentration change \( M_a \) and \( M_b \) and temperatures change \( T_a \) and \( T_b \) are assumed at the inside and outside of the disc, respectively. The unknown constants can be achieved using these hygrothermal boundary conditions as:

\[ W_1 = \frac{T_b - T_a}{\ln(b/a)}, \quad W_2 = \frac{T_b - T_a}{\ln(b/a)} \ln(b) - T_b. \]  
(3.a)

\[ S_1 = \frac{M_b - M_a}{\ln(b/a)}, \quad S_2 = \frac{M_b - M_a}{\ln(b/a)} \ln(b) - M_b. \]  
(3.b)

### 2.2 Basic equations of the MEE rotating disc

The entire strains are supposed to be sum of magnetic, electric, elastic, hygrothermal, and creep strains.

Therefore, the stress-strain relations can be written in the following form [25, 27]:

\[ \sigma_r = c_{11}(e_{rr} - \varepsilon^e_r) + c_{12}(e_{\theta\theta} - \varepsilon^e_{\theta}) + c_{13}(e_{zz} - \varepsilon^e_z) - e_{11}E_r - q_{11}H_r - \lambda_4T - \zeta_1M \]  
(4.a)

\[ \sigma_\theta = c_{12}(e_{rr} - \varepsilon^e_r) + c_{22}(e_{\theta\theta} - \varepsilon^e_{\theta}) + c_{23}(e_{zz} - \varepsilon^e_z) - e_{12}E_r - q_{12}H_r - \lambda_2T - \zeta_2M \]  
(4.b)

\[ \sigma_z = c_{13}(e_{rr} - \varepsilon^e_r) + c_{23}(e_{\theta\theta} - \varepsilon^e_{\theta}) + c_{33}(e_{zz} - \varepsilon^e_z) - e_{13}E_r - q_{13}H_r - \lambda_3T - \zeta_3M \]  
(4.c)

\[ D_r = e_{11}(e_{rr} - \varepsilon^e_r) + e_{12}(e_{\theta\theta} - \varepsilon^e_{\theta}) + e_{13}(e_{zz} - \varepsilon^e_z) + \beta_{11}E_r + \varepsilon_{11}H_r + pT + \chi_1M, \]  
(4.d)

\[ B_r = q_{11}(e_{rr} - \varepsilon^e_r) + q_{12}(e_{\theta\theta} - \varepsilon^e_{\theta}) + q_{13}(e_{zz} - \varepsilon^e_z) + \varepsilon_{11}E_r + d_{11}H_r + mT + \gamma_1M \]  
(4.e)

where...
\[ \lambda_1 = c_{11} \alpha_r + c_{12} \alpha_\theta + c_{13} \alpha_z \]
\[ \lambda_2 = c_{12} \alpha_r + c_{22} \alpha_\theta + c_{23} \alpha_z \]
\[ \lambda_3 = c_{13} \alpha_r + c_{23} \alpha_\theta + c_{33} \alpha_z \]  

(5.a)

\[ \zeta_1 = c_{11} \beta_r + c_{12} \beta_\theta + c_{13} \beta_z \]
\[ \zeta_2 = c_{12} \beta_r + c_{22} \beta_\theta + c_{23} \beta_z \]
\[ \zeta_3 = c_{13} \beta_r + c_{23} \beta_\theta + c_{33} \beta_z \]  

(5.b)

The equilibrium equation of the rotating MEE disc is presented as [14, 21]:

\[ \frac{\partial \sigma_r}{\partial r} + \frac{(\sigma_r - \sigma_\theta)}{r} + \rho r \omega^2 = 0. \]  

(6)

Without electric charge and electric current densities, the electrostatic and magnetostatic equations can be written as [14, 25]:

\[ \frac{\partial D_r}{\partial r} + \frac{D_r}{r} = 0, \]  

(7.a)

\[ \frac{\partial B_r}{\partial r} + \frac{B_r}{r} = 0. \]  

(7.b)

Two types of mechanical boundary condition are taken named Fixed-Free and Free-Free boundary conditions [22, 28]. Also, the inner and outer surface is subjected to electric potential and magnetic potential. These boundary conditions can be presented as:

Fixed – Free \[ u_r \bigg|_{r=a} = 0, \quad \sigma_r \bigg|_{r=b} = 0, \]
Free – Free \[ \sigma_r \bigg|_{r=a} = 0, \quad \sigma_r \bigg|_{r=b} = 0, \]
\[ \phi \bigg|_{r=a} = \phi_a, \quad \phi \bigg|_{r=b} = \phi_b, \]
\[ \psi \bigg|_{r=a} = \psi_a, \quad \psi \bigg|_{r=b} = \psi_b. \]  

(8)

Solving Eqs. (7), gives:

\[ D_r = \frac{A_1}{r}, \]  

(9.a)
\[ B_r = \frac{A_3}{r}, \quad (9.b) \]

where, \( A_1 \) and \( A_2 \) are unknown constants. Due to plane stress condition, the \( z \) component of stress is set to zero. So, we have:

\[
\sigma_z = 0 \Rightarrow (e_{zz} - e_{\theta\theta}) = -\frac{c_{12}}{c_{33}} (e_{\sigma} - e_{\sigma}) - \frac{c_{33}}{c_{33}} (e_{\phi\phi} - e_{\phi\phi}) + \frac{\epsilon_{11}}{c_{33}} E_r + \frac{\epsilon_{12}}{c_{33}} H_r + \frac{\lambda_1}{c_{33}} T + \frac{\zeta_2}{c_{33}} M
\]

(10)

Also, we know that:

\[
\varepsilon_{\sigma} = \frac{\partial u}{\partial r}, \quad \varepsilon_{\phi\phi} = \frac{u}{r}, \quad E_r = -\frac{\partial \phi}{\partial r}, \quad H_r = -\frac{\partial \psi}{\partial r}
\]

(11)

Using Eqs. (10) and (11), the Eqs. (4) can be rewritten as:

\[
\sigma_r = \epsilon'_{11} \frac{\partial u}{\partial r} + \epsilon'_{12} \frac{u}{r} + \varepsilon'_{11} \frac{\partial \phi}{\partial r} + \varepsilon'_{12} \frac{\partial \psi}{\partial r} - \lambda_1' T - \zeta_1' M - \epsilon'_{11} e_{\sigma} - \epsilon'_{12} e_{\sigma}\]

(12.a)

\[
\sigma_\phi = \epsilon'_{12} \frac{\partial u}{\partial r} + \epsilon'_{22} \frac{u}{r} + \varepsilon'_{12} \frac{\partial \phi}{\partial r} + \varepsilon'_{22} \frac{\partial \psi}{\partial r} - \lambda_2' T - \zeta_2' M - \epsilon'_{12} e_{\sigma} - \epsilon'_{22} e_{\sigma}\]

(12.b)

\[
D_r = \epsilon'_{11} \frac{\partial u}{\partial r} + \epsilon'_{12} \frac{u}{r} - \beta'_{11} \frac{\partial \phi}{\partial r} - \epsilon'_{11} \frac{\partial \psi}{\partial r} + p'T + \chi'_{1} M - \epsilon'_{11} e_{\sigma} - \epsilon'_{12} e_{\sigma}\]

(12.c)

\[
B_r = \epsilon'_{11} \frac{\partial u}{\partial r} + \epsilon'_{12} \frac{u}{r} - \epsilon'_{11} \frac{\partial \phi}{\partial r} - \epsilon'_{12} \frac{\partial \psi}{\partial r} + m'T + \gamma'_{1} M - \epsilon'_{11} e_{\sigma} - \epsilon'_{12} e_{\sigma}
\]

(12.d)

where
\[ c'_{11} = c_{11} - \frac{c_{13}^2}{c_{33}} \]
\[ c'_{12} = c_{12} - \frac{c_{13} c_{23}}{c_{33}} \]
\[ c'_{22} = c_{22} - \frac{c_{23}^2}{c_{33}} \]
\[ \chi' = \chi + \frac{e_{13} \zeta}{c_{33}} \]
\[ e'_{11} = e_{11} - \frac{c_{13} e_{13}}{c_{33}} \]
\[ e'_{12} = e_{12} - \frac{c_{13} e_{13}}{c_{33}} \]
\[ q'_{11} = q_{11} - \frac{c_{13} g_{13}}{c_{33}} \]
\[ q'_{12} = q_{12} - \frac{c_{23} g_{13}}{c_{33}} \]
\[ \lambda' = \gamma + \frac{g_{13}}{c_{33}} \]
\[ \lambda_2 = \gamma + \frac{g_{13}}{c_{33}} \]
\[ \zeta' = \frac{c_{13} \zeta}{c_{33}} \]
\[ \zeta_2 = \frac{c_{23} \zeta}{c_{33}} \]
\[ \gamma' = \gamma + \frac{g_{13}}{c_{33}} \]
\[ m' = m + \frac{\lambda_2 q_{13}}{c_{33}} \]
\[ d'_{11} = d_{11} + \frac{q_{13}^2}{c_{33}} \]
\[ \beta' = \beta + \frac{e_{13}^2}{c_{33}} \]
\[ \epsilon'_{11} = \epsilon_{11} + \frac{e_{13} g_{13}}{c_{33}} \]
\[ p' = p_1 + \frac{e_{13} \lambda_2}{c_{33}} \]

Substituting Eqs. (9) into Eq. (12.c) and (12.d), after rearranging, gives:

\[ \frac{\partial \phi(r)}{\partial r} = \left( L_1 \frac{\partial u}{\partial r} + L_2 \frac{u}{r} + L_3 \frac{A_1}{r} + L_4 T + L_5 M - L_6 A_1 \right) - L_7 \epsilon_{r} - L_8 \epsilon_{\theta} \]  
(14.a)

\[ \frac{\partial \psi(r)}{\partial r} = \left( P_1 \frac{\partial u}{\partial r} + P_2 \frac{u}{r} + P_3 \frac{A_1}{r} + P_4 T + P_5 M - P_6 \right) - P_7 \epsilon_{r} - P_8 \epsilon_{\theta} \]  
(14.b)

Where:

\[ L_1 = \frac{e_{11} d_{11} - e_{11} q_{11}}{\beta_1 d_{11} - e_{11}^2} \]
\[ L_2 = \frac{e_{12} d_{11} - e_{12} q_{12}}{\beta_1 d_{11} - e_{11}^2} \]
\[ L_3 = \frac{e_{11}}{\beta_1 d_{11} - e_{11}^2} \]
\[ L_4 = \frac{d_{11} p' - e_{11} m'}{\beta_1 d_{11} - e_{11}^2} \]
\[ L_5 = \frac{d_{11}}{\beta_1 d_{11} - e_{11}^2} \]
\[ L_6 = \frac{q_{11} \beta_1 - e_{11} e_{11}^2}{\beta_1 d_{11} - e_{11}^2} \]
\[ P_1 = \frac{q_{11} \beta_1 - e_{11} e_{11}^2}{\beta_1 d_{11} - e_{11}^2} \]
\[ P_2 = \frac{q_{12} \beta_1 - e_{12} e_{11}^2}{\beta_1 d_{11} - e_{11}^2} \]
\[ P_3 = \frac{e_{11}}{\beta_1 d_{11} - e_{11}^2} \]
\[ P_4 = \frac{\epsilon_{11} m'}{\beta_1 d_{11} - e_{11}^2} \]
\[ P_5 = \frac{\epsilon_{11} p'}{\beta_1 d_{11} - e_{11}^2} \]
\[ P_6 = \frac{\epsilon_{11} \lambda_2}{\beta_1 d_{11} - e_{11}^2} \]

Substituting Eq. (14) into Eqs. (12.a) and (12.b) gives:

\[ \sigma_r = C_1 \frac{\partial u}{\partial r} + C_2 \frac{u}{r} + C_3 \frac{A_1}{r} + C_4 \frac{A_1}{r} + C_5 T + C_6 M - \lambda_1' T - \zeta_1' M - C_1 \epsilon_r - C_2 \epsilon_{\theta} \]  
(16.a)

\[ \sigma_\theta = E_1 \frac{\partial u}{\partial r} + E_2 \frac{u}{r} + E_3 \frac{A_1}{r} + E_4 \frac{A_1}{r} + E_5 T + E_6 M - \lambda_2' T - \zeta_2' M - E_1 \epsilon_r - E_2 \epsilon_{\theta} \]  
(16.b)

where,
Substituting Eqs. (16) into Eq. (6), the equilibrium equation is now can be expressed as:

\[
\frac{\partial^2 u}{\partial r^2} + \frac{1}{r} \frac{\partial u}{\partial r} + \frac{1}{r^2} M \mu = +M_\mu r^{-1} T + M_4 \frac{T}{r} + \left( M_5 + M_6 \right) \frac{\partial T}{\partial r} + \frac{A_2}{r^2} + M_8 \frac{A_1}{r^2} + M_9 r^{-1} M + M_{10} \frac{M}{r} + \left( -M_{11} + M_{12} \right) \frac{\partial M}{\partial r} - M_1 r \\
+ M_{14} r^{-1} \varepsilon_r + \frac{\partial \varepsilon_r}{\partial r} + M_{15} r^{-1} \varepsilon_\theta + M_6 \frac{\partial \varepsilon_\theta}{\partial r}
\]

where,

\[
M_1 = \frac{C_1 + C_2 - E_{11}}{C_1}, \quad M_2 = \frac{-E_{22}}{C_1}, \quad M_3 = \frac{\lambda_1 - \lambda_2}{C_1}, \quad M_4 = \frac{E_1 - C_1}{C_1}, \\
M_5 = \frac{C_2}{C_1}, \quad M_6 = \frac{\lambda_1}{C_1}, \quad M_7 = \frac{E_2}{C_1}, \quad M_8 = \frac{E_4}{C_1}, \quad M_9 = \frac{\varepsilon_r}{C_1}, \quad M_10 = \frac{E_5 - C_1}{C_1}, \\
M_{11} = \frac{C_3}{C_1}, \quad M_{12} = \frac{\varepsilon_\theta}{C_1}, \quad M_{13} = \frac{\rho \omega^2}{C_1}, \quad M_{14} = \frac{2C_1 - 2E_1}{C_1}, \quad M_{15} = \frac{2C_2 - 2E_2}{C_1}, \quad M_{16} = \frac{C_3}{C_1}
\]

3. Solution of the equations

3.1 Primitive hygrothermal analysis of the MEE rotating disc

To find initial stresses, eliminating creep strains in the differential equation of Eq. (28), we have:

\[
\frac{\partial^2 u}{\partial r^2} + \frac{M_1}{r} \frac{\partial u}{\partial r} + \frac{M_2}{r^2} u = \left( -M W_1 - M_9 S_2 - M W_2 - M_{10} S_1 - M_1 S_1 + M_{12} S_2 \right) r^{-1} \\
+ \left( W_1 M_1 + S_1 M_9 + W_1 M_4 + S_1 M_{10} \right) \ln(r) r^{-1} + M_2 A_2 r^{-2} + M_4 A_1 r^{-2} - M_1 r
\]

The complete solution of Eq. (20) may be considered as:
\[ u = B_1 r^{m_1} + B_2 r^{m_2} + B_3 r + B_4 r^3 + B_5 A_2 + B_6 A_1 - \frac{B_7 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} \right) \]
\[ + \frac{B_8 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} \right) \]

Where \( B_1 \) and \( B_2 \) are unknown constants and:

\[
m_{1,2} = \frac{1}{2} \left( (M_1 - 1) \pm \sqrt{(M_1 - 1)^2 - 4M_2} \right), \quad B_8 = \frac{M_7}{M_2}, \quad B_7 = \frac{M_7}{M_2}, \]
\[
B_5 = -M_4 W_2 - M_9 W_3 - M_9 W_3 - M_9 W_4 - M_9 S_3 - M_9 W_4, \quad B_6 = \frac{-M_{13}}{6 + 3M_4 + M_2},
\]

Using Eq. (21) in Eq. (14.4) and then integrating, one has:

\[
\phi(r) = L_1 \left( B_1 r^{m_1} + B_2 r^{m_2} + B_3 r + B_4 r^3 - \frac{B_5 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - 2r - \frac{r}{1-m_1} \right) \right) - \frac{B_5 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - 2r - \frac{r}{1-m_1} \right) + L_2 \left( \frac{B_5 r}{m_1} + B_5 r^{m_2} + B_5 - \frac{B_5 r^3}{3} + (B_5 A_2 + B_5 A_1) \ln(r) \right) - \frac{B_5 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - 1 - \frac{1}{1-m_2} \right) + \frac{B_5 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - 1 - \frac{1}{1-m_2} \right) + L_3 (W_1 \ln(r) - W_1 + W_2, r) + L_4 (S_1 \ln(r) - S_1, r + S_1, r) + (L_5 A_1 + L_5 A_1) \ln(r) + Z_1,
\]

Where, \( Z_1 \) is an unknown constant. With a similar method, \( \psi(r) \) is achieved as:

\[
\psi(r) = P_1 \left( B_1 r^{m_1} + B_2 r^{m_2} + B_3 r + B_4 r^3 - \frac{B_5 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - 2r - \frac{r}{1-m_1} \right) \right) - \frac{B_5 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - 2r - \frac{r}{1-m_1} \right) + P_2 \left( \frac{B_5 r}{m_1} + B_5 r^{m_2} + B_5 - \frac{B_5 r^3}{3} + (B_5 A_2 + B_5 A_1) \ln(r) \right) - \frac{B_5 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - 1 - \frac{1}{1-m_2} \right) + \frac{B_5 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - 1 - \frac{1}{1-m_2} \right) \]

where, \( Z_2 \) is an unknown constant. Using Eq. (21) and Eqs. (2) into Eqs. (16), the radial and hoop stresses are achieved as:
\[
\sigma_r = C_i \left( B_1 m_1 r^{-m_1} + B_2 m_2 r^{-m_2} + B_3 + 3 \nu r^2 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} + 1 \right) \right) \\
+ \frac{B_5}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} + 1 \right) + C_i \left( B_1 m_1 r^{-m_1} + B_2 m_2 r^{-m_2} + B_3 r + 3 \nu r^3 + B_4 A_2 + B_4 A_1 \right) \\
- \frac{B_3 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} + 1 \right) + \frac{B_5 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} \right) \\
+ C_i \frac{A_2}{r} + C_i \frac{A_1}{r} + (C_5 - \lambda_r) (W_1 \ln(r) + W_2) + (C_6 - \zeta_r) (S_1 \ln(r) + S_2) 
\]

\[
\sigma_\theta = E_i \left( B_1 m_1 r^{-m_1} + B_2 m_2 r^{-m_2} + B_3 + 3 \nu r^2 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} + 1 \right) \right) \\
+ \frac{B_5}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} + 1 \right) + E_i \left( B_1 m_1 r^{-m_1} + B_2 m_2 r^{-m_2} + B_3 r + 3 \nu r^3 + B_4 A_2 + B_4 A_1 \right) \\
- \frac{B_3 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} + 1 \right) + \frac{B_5 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} \right) \\
+ E_i \frac{A_2}{r} + E_i \frac{A_1}{r} + (E_5 - \lambda_r) (W_1 \ln(r) + W_2) + (E_6 - \zeta_r) (S_1 \ln(r) + S_2) 
\]

The unknown constants \( A_i, A_2, B_1, B_2, Z_1 \) and \( Z_2 \) can be determined by employing the magneto-electro-mechanical boundary conditions. The boundary conditions result in a system of six linear algebraic equations. These six algebraic equations are expressed in the form as:

\[
X \begin{bmatrix} B_1 & B_2 & A_1 & A_2 & Z_1 & Z_2 \end{bmatrix} = E 
\]

Where, the component of matrix \( X \) and \( E \) are presented in the Appendix. Solving the system of equations results in obtaining the initial stresses, electric potential, magnetic potential and radial displacement analytically at zero time.

### 3.2 Creep analysis of MEE rotating disc

Considering the steady-state hygrothermal condition, differentiation Eq. (18) with respect to time yields:

\[
\frac{\partial^2 \hat{u}}{\partial \theta^2} + \frac{1}{r^2} \frac{\partial \hat{u}}{\partial r} + \frac{1}{r^2} M \hat{u} = + M \frac{\dot{A}_2}{r^2} + M \frac{\dot{A}_1}{r^2} + M \frac{\dot{\epsilon}_{\theta \theta}}{r^2} + M \frac{\dot{\epsilon}_{\theta \phi}}{r^2} + M \frac{\dot{\epsilon}_{\phi \phi}}{r^2} + M \frac{\dot{\epsilon}_{\theta \phi}}{r^2} + M \frac{\dot{\epsilon}_{\phi \phi}}{r^2} 
\]

Well-known Prandtl-Reuss equations relate the creep rates to the stresses as follows [27]:

\[
\frac{\partial^2 \hat{u}}{\partial \theta^2} + \frac{1}{r^2} \frac{\partial \hat{u}}{\partial r} + \frac{1}{r^2} M \hat{u} = + M \frac{\dot{A}_2}{r^2} + M \frac{\dot{A}_1}{r^2} + M \frac{\dot{\epsilon}_{\theta \theta}}{r^2} + M \frac{\dot{\epsilon}_{\theta \phi}}{r^2} + M \frac{\dot{\epsilon}_{\phi \phi}}{r^2} + M \frac{\dot{\epsilon}_{\theta \phi}}{r^2} + M \frac{\dot{\epsilon}_{\phi \phi}}{r^2} 
\]
\[
\varepsilon_r^c = \frac{\dot{\varepsilon}_r^c}{\sigma_r} (\sigma_r - 0.5(\sigma_\theta + \sigma_z)) \\
\varepsilon_\theta^c = \frac{\dot{\varepsilon}_\theta^c}{\sigma_\theta} (\sigma_\theta - 0.5(\sigma_r + \sigma_z)) \\
\varepsilon_z^c = \frac{\dot{\varepsilon}_z^c}{\sigma_z} (\sigma_z - 0.5(\sigma_\theta + \sigma_r))
\]  

(29)

Where \( \varepsilon_i^c \) (i = r, \theta, \phi) is creep strain rate, \( \dot{\varepsilon}_c^c \) is effective creep strain rate and \( \sigma_c \) is effective stress. Norton's law is considered as the creep constitutive model as [27]:

\[
\dot{\varepsilon}_c^c = B(r)\sigma_c^{n(r)}
\]  

(30)

Where material creep parameters \( B(r) \) and \( n(r) \) are function of radius as [27]:

\[
B(r) = b_0 r^{b_1}, \quad n(r) = n_0
\]  

(31)

Where \( b_0, b_1 \) and \( n_0 \) are constants. Regarding the plane stress condition and substituting Eq. (30) into Eqs. (29) gives:

\[
\varepsilon_r^c = b_0 r^{b_1} \sigma_c^{n-1} (\sigma_r - .5\sigma_\theta) \\
\varepsilon_\theta^c = b_0 r^{b_1} \sigma_c^{n-1} (\sigma_\theta - .5\sigma_r) \\
\varepsilon_z^c = -(\varepsilon_r^c + \varepsilon_\theta^c)
\]  

(32)

The Von Mises equivalent stress is presented as:

\[
\sigma_c = \sqrt{\sigma_r^2 + \sigma_\theta^2 - \sigma_r \sigma_\theta}
\]  

(33)

By the same way as in previous section, the solution of Eq. (28) can be considered as:

\[
\dot{u} = D_1 r^{m_1} + D_2 r^{m_2} + G_1 r^{m_3} + G_2 r^{m_4} + B_7 \dot{A}_2 + B_8 \dot{A}_1
\]  

(34)

where \( G_1(r) \) and \( G_2(r) \) can be achieved using the method of variation of parameters as [21]:
\[ G_{11}(r) = \frac{\sqrt{3}}{2} \frac{b_0}{m_2 - m_1} \int \left\{ r^{b_1 - m_1} \sigma_e^{m_0} \left( M_{15} + M_{16}b_1 - M_{14} - b_1 \right) + (M_{16} - 1) r^{b_1 - m_1 + 1} \frac{\partial \sigma_e^{m_0}}{\partial r} \right\} dr \]
\[ G_{21}(r) = -\frac{\sqrt{3}}{2} \frac{b_0}{m_2 - m_1} \int \left\{ r^{b_1 - m_2} \sigma_e^{m_0} \left( M_{15} + M_{16}b_1 - M_{14} - b_1 \right) + (M_{16} - 1) r^{b_1 - m_2 + 1} \frac{\partial \sigma_e^{m_0}}{\partial r} \right\} dr \]

Now, rates of stresses, electric potential and magnetic potential can be gotten by differentiation Eqs. (14) and (16) with respect to time as:

\[ \dot{\sigma}_r = C_1 \frac{\partial \tilde{u}}{\partial r} + C_2 \frac{\tilde{u}}{r} + C_3 \frac{A_2}{r} + C_4 \frac{\dot{A}_1}{r} - C_1 \dot{e}^{\sigma}_{\tau \tau} - C_2 \dot{e}^{\sigma}_{\theta \theta}, \]  
(36.a)

\[ \dot{\sigma}_\theta = E_1 \frac{\partial \tilde{u}}{\partial r} + E_2 \frac{\tilde{u}}{r} + E_3 \frac{A_2}{r} + E_4 \frac{\dot{A}_1}{r} - E_1 \dot{e}^{\sigma}_{\tau \tau} - E_2 \dot{e}^{\sigma}_{\theta \theta}, \]  
(36.b)

\[ \ddot{\phi} = L_1 \frac{\partial \tilde{u}}{\partial r} + L_2 \frac{\tilde{u}}{r} + L_3 \frac{A_2}{r} - L_1 \frac{\dot{A}_1}{r} - L_2 \dot{e}^{\sigma}_{\tau \tau} - L_2 \dot{e}^{\sigma}_{\theta \theta}, \]  
(36.c)

\[ \ddot{\psi} = P_1 \frac{\partial \tilde{u}}{\partial r} + P_2 \frac{\tilde{u}}{r} + P_3 \frac{A_2}{r} - P_2 \frac{\dot{A}_1}{r} - P_2 \dot{e}^{\sigma}_{\tau \tau} - P_2 \dot{e}^{\sigma}_{\theta \theta}, \]  
(36.d)

Substituting Eq. (34) into Eqs. (36) and integrating Eqs. (36.c) and (36.d), after rearranging, gives:

\[ \dot{\sigma}_r = D_1 \left( (m_1 C_1 + C_2) r^{m_1 - 1} \right) + D_2 \left( (m_2 C_1 + C_2) r^{m_1 - 1} \right) + \left( C_2 B_1 + C_4 \right) \frac{\dot{A}_1}{r} \]  
(37.a)

\[ + \left( C_1 B_1 + C_3 \right) \frac{\dot{A}_2}{r} - C_2 \left( \frac{\partial G_{11}}{\partial r} r^{m_1} + G_1 m_1 r^{m_1 - 1} + \frac{\partial G_{21}}{\partial r} r^{m_2} + G_2 m_2 r^{m_2 - 1} \right) \]  

\[ + C_2 \left( G_1 r^{m_1} + G_2 r^{m_2} \right) - b_0 r^{m_1} \sigma_e^{m_1} \left( E_1 \left( \sigma_r - 5 \sigma_\theta \right) + E_2 \left( \sigma_\theta - 5 \sigma_r \right) \right) \]  

\[ \dot{\sigma}_\theta = D_1 \left( (m_1 C_1 + C_2) r^{m_1 - 1} \right) + D_2 \left( (m_2 C_1 + C_2) r^{m_1 - 1} \right) + \left( E_1 B_1 + E_4 \right) \frac{\dot{A}_1}{r} \]  
(37.b)

\[ + \left( E_2 B_1 + E_3 \right) \frac{\dot{A}_2}{r} - E_2 \left( \frac{\partial G_{11}}{\partial r} r^{m_1} + G_1 m_1 r^{m_1 - 1} + \frac{\partial G_{21}}{\partial r} r^{m_2} + G_2 m_2 r^{m_2 - 1} \right) \]  

\[ + E_2 \left( G_1 r^{m_1} + G_2 r^{m_2} \right) - b_0 r^{m_1} \sigma_e^{m_1} \left( E_1 \left( \sigma_r - 5 \sigma_\theta \right) + E_2 \left( \sigma_\theta - 5 \sigma_r \right) \right) \]  

\[ \dot{\phi} = D_1 \left( L_1 + L_2 \right) + \frac{D_1}{m_1} \left( L_1 + \frac{L_2}{m_2} \right) - (B_1 \ln(r) + (B_2 + L_3) \ln(r) \dot{A}_1 \right) \]  
(37.c)

\[ + \int \left( \frac{\partial G_{11}}{\partial r} r^{m_1} + G_1 m_1 r^{m_1 - 1} + \frac{\partial G_{21}}{\partial r} r^{m_2} + G_2 m_2 r^{m_2 - 1} \right) + L_2 \left( G_1 r^{m_1} + G_2 r^{m_2} \right) - L_2 \dot{e}^{\sigma}_{\tau \tau} - L_2 \dot{e}^{\sigma}_{\theta \theta} \right) dr + J_1 \]
\[ \dot{y} = D_1 r^{m_1} \left( P_1 + \frac{P_2}{m_1} \right) + D_2 r^{m_2} \left( P_1 + \frac{P_2}{m_2} \right) - \left( B_s(z_2) + P_s \right) r^{-\beta} A_1 - \left( B_s(z_2) - P_s \right) \ln(r) A_2 \]

\[ + \int \left[ \left( \frac{\partial G_1}{\partial r} r^{m_1} + G_1 m_1 r^{m_1-1} + \frac{\partial G_2}{\partial r} r^{m_2} + G_2 m_2 r^{m_2-1} \right) + P_s \left( + G_1 r^{m_1-1} + G_2 r^{m_2-1} \right) - P_s \dot{\epsilon}_e - P_s \dot{\epsilon}_e \right] dr + J_2 \]

Using the boundary conditions, the unknown constants can be determined. The boundary condition of inner and outer radii of the MEE disc does not vary with the time, so there:

\[ \begin{align*}
\text{Fixed} - \text{Free} & \rightarrow \dot{u}_r \bigg|_{r=a} = 0, \quad \dot{\sigma}_r \bigg|_{r=b} = 0, \\
\text{Free} - \text{Free} & \rightarrow \sigma_r \bigg|_{r=a} = 0, \quad \sigma_r \bigg|_{r=b} = 0, \\
& \dot{\phi}_r \bigg|_{r=a} = 0, \quad \dot{\phi}_r \bigg|_{r=b} = 0, \\
& \psi_r \bigg|_{r=a} = 0, \quad \psi_r \bigg|_{r=b} = 0. \\
\end{align*} \]

The resultant system of linear equations can be solved like as previous section. The details are presented in the Appendix. To achieve history of stresses, electric and magnetic potential during creep progress, the rates of stresses, electric potential and magnetic potential are needed. First of all, a suitable time increment \((dt^{(i)})\) needs to be taken. The entire time is the sum of timing steps as the creep evolutions during the time. The total time after the \(i\)th timing step can be presented as:

\[ t_i = \sum_{k=0}^{i} dt^{(k)} \]

In the following time steps, the radial and hoop stress redistributions for former step are available, and then, the radial and hoop stress rates are acquired from Eqs. (37.a) and (37.b). Lastly, using an iterative method, the creep stress distribution can be achieved as:

\[ \begin{align*}
\sigma_r^{(i)}(r, t_j) &= \sigma_r^{(i-1)}(r, t_{j-1}) + \sigma_r^{(i-1)}(r, t_{j-1}) dt^{(i)} \\
\sigma_\theta^{(i)}(r, t_j) &= \sigma_\theta^{(i-1)}(r, t_{j-1}) + \sigma_\theta^{(i-1)}(r, t_{j-1}) dt^{(i)}
\end{align*} \]

4. Numerical results and discussions
In this section, employing MATLAB software, the influence of various parameters on the creep response of MEE disc is investigated using some numerical examples. Material constants for the MEE can be found in Table 1 [5, 27]. The inner radii \(a = 0.04\,\text{m}\) and outer radii \(b = 0.15\,\text{m}\) are taken for the disc. The following non-dimensional quantities are used for the numerical results:

\[
R = \frac{r - a}{b - a}, \quad u^* = \frac{u(r)}{a}, \quad \sigma^*_i = \frac{\sigma_i}{P_a}, (i = r, \theta), \quad \phi^* = \sqrt{\frac{\beta_{11} \phi(r)}{c_{11} b}}, \quad \psi^* = \sqrt{\frac{d_{11} \psi(r)}{c_{11} b}}.
\]  

(41)

Firstly, the creep evolution during the time is investigated. The boundary conditions are supposed as:

\[
\phi_a = 0, \quad \phi_b = 5000, \quad \psi_a = 0, \quad \psi_b = 0, \quad T_a = 0, \quad T_b = 50, \quad M_a = 0, \quad M_b = 0.5, \quad \omega = 30\pi.
\]  

(42)

Figs. 2-7 show the creep evolution of MEE disc under multiphysical loading for the Free-Free mechanical boundary condition. In this analysis, time increment \(dt = 5 \times 10^4\,\text{s}\) is used. It is observed that radial stress, electric potential and magnetic potential are constant during the time at the inner and outer radii of disc which satisfy the constant electro-magneto-mechanical boundary conditions. Concerning to Fig. 2, the tensile radial stress decreases with the time. Also, the location of maximum radial stress is changed during the time. Fig. 3 shows that the absolute value of circumferential stress is decreasing with time at the internal and external surface of the MEE disc during the time. Also, the location of maximum hoop stress is moved from internal surface toward middle of thickness. Fig. 4 illustrates that the effective stress is decreased with time significantly. Besides, the distribution of equivalent stress through the thickness becomes more uniform during the creep progress. Fig. 5 illustrates that the displacement rises with serving the time. According to Fig. 6, the maximum electric potential is decreased during the creep evolution. Since the disc is radially polarized, the radial stress redistribution has some effects on the electric potential distribution. Consequently, with the aim of condition monitoring, the electric potential histories may be used in the intelligent disc. Fig. 7 shows that the creep evolution has not a significant effect on the distribution of magnetic potential.
Table 1. Material constants.

<table>
<thead>
<tr>
<th>$c_{11} (GPa)$</th>
<th>$c_{12} (GPa)$</th>
<th>$c_{23} (GPa)$</th>
<th>$c_{22} (GPa)$</th>
<th>$e_{11} (C/m^2)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>215</td>
<td>120</td>
<td>120</td>
<td>218</td>
<td>7.5</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>$e_{12} (C/m^2)$</th>
<th>$\alpha_r (1/K)$</th>
<th>$\alpha_\theta (1/K)$</th>
<th>$q_{11} (N/Am)$</th>
<th>$q_{12} (N/Am)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>-2.5</td>
<td>6x10^{-6}</td>
<td>15x10^{-6}</td>
<td>345</td>
<td>265</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>$\beta_{11} (C^2/N m^2)$</th>
<th>$d_{11} (Ns^2/C^2)$</th>
<th>$\varepsilon_{11} (Ns/IVC)$</th>
<th>$\beta_r (m^3/kg)$</th>
<th>$\beta_\theta (m^3/kg)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>5.8x10^{-9}</td>
<td>95x10^{-6}</td>
<td>2.82x10^{-9}</td>
<td>0.8x10^{-4}</td>
<td>1.2x10^{-4}</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>$m_1 (N/AmK)$</th>
<th>$\chi_1 (Cm/kg)$</th>
<th>$P_1 (C^2/m^2k)$</th>
<th>$\gamma_1 (Nm^2/Akg)$</th>
<th>$n_0$</th>
</tr>
</thead>
<tbody>
<tr>
<td>2.5x10^{-5}</td>
<td>0</td>
<td>-2.5x10^{-5}</td>
<td>0</td>
<td>3</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>$b_1$</th>
<th>$b_0$</th>
</tr>
</thead>
<tbody>
<tr>
<td>-5</td>
<td>0.11x10^{-36}</td>
</tr>
</tbody>
</table>

Fig. 2. Radial stress redistribution during creep progress (Free-Free)
Fig. 3. Hoop stress redistribution during creep progress (Free-Free)

Fig. 4. Equivalent stress redistribution during creep progress (Free-Free)

Fig. 5. Radial Displacement redistribution during creep progress (Free-Free)
Fig. 6. Electric potential redistribution during creep progress (Free-Free)

Fig. 7. Magnetic Potential redistribution during creep progress (Free-Free)

Figs. 8-10 show the creep evolution of MEE disc for the Fixed-Free mechanical boundary condition. Other boundary conditions are as before case. It is observed that radial stress at the outer radii as well as the radial displacement at the inner radii is constant during the time which satisfies the Fixed-Free boundary conditions. Regarding Fig. 8, the tensile radial stress decreases with the time. Also, during the time, the location of maximum radial stress is changed from inner radii to middle of thickness approximately. Fig. 9 shows that the general behavior of hoop stress of the MEE disc during the time is similar to the previous case. Fig. 10 depicts that the radial displacement rises during the time. The enhancement is more considerable at outer radii.
Fig. 8. Radial stress redistribution during creep progress (Fixed-Free)

Fig. 9. Hoop stress redistribution during creep progress (Fixed-Free)

Fig. 10. Radial Displacement redistribution during creep progress (Fixed-Free)
The effect of temperature and humidity on the primitive and creep behavior of the MEE disc is disclosed in Figs. 11-15. The temperature and moisture concentration on the interior surface are taken as zero. However, the temperature and moisture concentration rise on the exterior surface \((M_b=T_b/100)\). The Free-Free boundary condition is taken and other boundary conditions are same as before. According to Fig. 11, increasing in hygrothermal loading rises the tensile radial stress both for primitive and after creep evolution. Furthermore, changes in primitive radial stress are more significant rather than creep one.

Fig. 11. Effect of hygrothermal loading on the initial and creep radial stress

Fig. 12 depicts that, for primitive state, there is a fix point near the middle of thickness in which the circumferential stress does not change with change in hygrothermal loading. Before this point, rising in hygrothermal loading increases the tensile circumferential stress. While, after this point, it increases the compressive hoop stress. This enhancement must be considered in designing of MEE disc because high tensile hoop stress provides proper opportunity for cracking at the inner surface of MEE disc. The effect of hygrothermal loading on the hoop stress after creep evolution is insignificant according to Fig. 12. As observed in Fig. 13, for the primitive state, the effective stress is increased by increasing in hygrothermal loading. While, for the creep state, the effect of hygrothermal condition is inconsiderable. Fig. 14 reveals
that an increase in applied hygrothermal loading results in an increase in both primitive and creep radial displacements. Fig. 15 demonstrated that rising in temperature and moisture concentration increases the maximum of electric potential for both initial and after creep evolution. The changes are more extensive in primitive case. In general, Fig. 11-15 implies that the effect of hygrothermal loading condition after creep evolution becomes less significant comparison with the static case.

Fig. 12. Effect of hygrothermal loading on the initial and creep hoop stress

Fig. 13. Effect of hygrothermal loading on the initial and creep equivalent stress
For the next case, the influence of angular speed on the creep behavior is considered. The results are demonstrated in Fig. 16-19. Fig. 16 and 17 show that increasing in angular velocity has no considerable effect on the creep radial and hoop stresses. While, it increases the static radial and hoop stresses at increasing rate. According to Fig. 18, as the angular velocity rises, the initial effective stress increases at an increasing rate in the internal surface and decreases in the external surface. The angular velocity has no considerable effect on the effective creep stress. Fig. 19 depicts that increasing in angular velocity leads to an increase radial displacement in both initial and creep state. It can be concluded from Figs. 16-19 that generally the effect of angular velocity becomes less significant after creep progress.
Fig. 16. Effect of speed of rotation on the initial and creep radial stress

Fig. 17. Effect of speed of rotation on the initial and creep hoop stress

Fig. 18. Effect of speed of rotation on the initial and creep equivalent stress
To explore the influence of temperature- and moisture- dependent elastic coefficients on the response of MEE disc, the elastic coefficients can be expressed in the following form [25]:

$$C_{ij} = C_{ij0} (1 + \alpha^T T + \beta^M M)$$  \hspace{1cm} (43)

To avoid having non-linear equations, the temperature and moisture dependence is only assumed for the case that temperature and moisture concentration increase uniformly. So, the temperature and moisture concentration increases uniformly as: $T=50$, $M=0.5$. The Free-Free boundary condition is taken and other boundary conditions are kept unchanged. Fig. 20-23 reveals the influence of the hygrothermal dependence of the elastic coefficients on the initial and creep response of the MEE disc. Due to similarity of the effect of the temperature and humidity on the multiphysical behavior, the similar values are used for the empirical constants of temperature and moisture dependence. It is obvious that $\alpha^T=\beta^M=0$ indicates the material properties are independent of temperature and moisture. As shown in Fig. 20-23, the empirical constant has a negligible effect on the distribution of initial stresses and radial displacement of MEE disc. Fig. 20 shows that a positive empirical constant results in a reduction of creep radial stress. While, the effect of a minus value of empirical constant is vice versa. Fig. 21 depicts that the positive empirical constant reduces both the compressive creep hoop stress at the outer radii and tensile creep hoop stress at the inner radii. While, a negative empirical constant has an opposite influence. Fig. 22 shows the creep equivalent stress rises (decreases) using negative (positive) value of empirical constant.
Fig. 20. Effect of hygrothermal dependency on the initial and creep radial stress

Fig. 21. Effect of hygrothermal dependency on the initial and creep hoop stress

Fig. 22. Effect of hygrothermal dependency on the initial and creep equivalent stress
As observed in Fig. 23, using a positive empirical constant result in a reduction in radial displacement. While, using a negative one has a reverse effect. It can be concluded from Figs. 16-19 that analysis of the effect of temperature and moisture dependence after creep evolution is more important rather than initial state and it must be considered in the design progress.

5. Conclusion

In this article, a magneto-electro-elastic rotating disc subjected to an axisymmetric hygro-thermo-magneto-mechanical loading is considered. Applying the Prandtl-Reuss equations and Norton’s law, the time-dependent creep behavior of the disk is analyzed analytically for the first time. The following conclusions can be expressed from the results:

1. The radial stress and absolute value of hoop stress decrease with the time in both Fixed-Free and Free-Free boundary conditions. While the radial displacement rises with serving the time.

2. Increasing in hygrothermal loading rises the initial radial stress, equivalent stress, radial displacement and maximum electric potential. Also, it increases the tensile hoop stress at the internal surface. Thus, to avoid cracking, this enhancement must be considered in design progress.

3. Increasing in angular velocity increases the initial radial and hoop stresses in addition to radial displacement at increasing rate.
4. Generally, the effect of hygrothermal loading and angular velocity becomes less significant after creep evolution comparison with static case.

5. Positive empirical constant of temperature- and moisture- dependency yields to a decrease in radial stress, absolute value of hoop stress, equivalent stress and radial displacement after creep evolution, while the negative value has an opposite effect.

6. The results imply that the effect of temperature- and moisture- dependence after creep evolution is more considerable and must be considered in the design progress.

Appendix

The component of matrix $X$ and $E$ for the primitive state with Free-Free boundary condition can be expressed as:

$$X_{11} = (C_1m_1 + C_2)a^{m_1-1}, \quad X_{12} = (C_1m_2 + C_2)a^{m_2-1}, \quad X_{13} = \frac{C_3 + C_2B_8}{a}, \quad X_{14} = \frac{C_3 + C_2B_7}{a},$$

$$X_{15} = X_{16} = 0$$

$$X_{21} = (C_1m_1 + C_2)b^{m_1-1}, \quad X_{22} = (C_1m_2 + C_2)b^{m_2-1}, \quad X_{23} = \frac{C_4B_3 + C_4}{b}, \quad X_{24} = \frac{C_2B_7 + C_3}{b},$$

$$X_{25} = X_{26} = 0$$

$$X_{31} = a^{m_1}\left(\frac{L_2}{m_1} + L_1\right), \quad X_{32} = a^{m_2}\left(\frac{L_2}{m_2} + L_1\right), \quad X_{33} = (-L_5 + L_2B_8)\ln(a),$$

$$X_{34} = (L_3 + L_2B_7)\ln(a), X_{35} = 1, \quad X_{36} = 0$$

$$X_{41} = b^{m_1}\left(\frac{L_2}{m_1} + L_1\right), \quad X_{42} = b^{m_2}\left(\frac{L_2}{m_2} + L_1\right), \quad X_{43} = (-L_5 + L_2B_8)\ln(b),$$

$$X_{44} = (L_3 + L_2B_7)\ln(b), X_{45} = 1, \quad X_{46} = 0$$

$$X_{51} = a^{m_1}\left(P_1 + \frac{P}{m_1}\right), \quad X_{52} = a^{m_2}\left(P_1 + \frac{P}{m_2}\right), \quad X_{53} = (-P_3 + P_2B_8)\ln(a),$$

$$X_{54} = (P_3 + P_2B_7)\ln(a), X_{55} = 0, \quad X_{56} = 1$$

$$X_{61} = b^{m_1}\left(P_1 + \frac{P}{m_1}\right), \quad X_{62} = b^{m_2}\left(P_1 + \frac{P}{m_2}\right), \quad X_{63} = (-P_3 + P_2B_8)\ln(b),$$

$$X_{64} = (P_3 + P_2B_7)\ln(b), X_{65} = 0, \quad X_{66} = 1$$
\[
E = \begin{bmatrix}
-S_i(a) \\
-S_i(b) \\
\phi_a - S_2(a) \\
\phi_b - S_2(b) \\
\psi_a - S_3(a) \\
\psi_b - S_3(b)
\end{bmatrix}
\]

\[
S_1 = C_1 \left( B_3 + 3B_6r^2 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} + 1 \right) \right)
+ \frac{B_5}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} + 1 \right) + C_2 \left( B_3r + B_6r^3 + B_7A_2 + B_8A_4 \right)
\]

\[
S_1 = C_1 \left( B_3 + 3B_6r^2 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} + 1 \right) \right)
+ \frac{B_5}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} + 1 \right) + C_2 \left( B_3r + B_6r^3 + B_7A_2 + B_8A_4 \right)
\]

\[
S_2 = L_1 \left( B_3r + B_5 + B_6r^3 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_1} \right) \right)
- \frac{B_5}{(1-m_2)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_2} \right) + L_2 \left( B_3r + \frac{B_6}{3}r^3 \right)
\]

\[
S_2 = L_1 \left( B_3r + B_5 + B_6r^3 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_1} \right) \right)
- \frac{B_5}{(1-m_2)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_2} \right) + L_2 \left( B_3r + \frac{B_6}{3}r^3 \right)
\]

\[
S_3 = \psi(r) = P_1 \left( B_3r + B_5 + B_6r^3 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_1} \right) \right)
- \frac{B_5}{(1-m_2)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_2} \right) + P_2 \left( B_3r + \frac{B_6}{3}r^3 \right)
\]

\[
S_3 = \psi(r) = P_1 \left( B_3r + B_5 + B_6r^3 - \frac{B_5}{(1-m_1)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_1} \right) \right)
- \frac{B_5}{(1-m_2)(m_2-m_1)} \left( r \ln(r) - 2r\frac{r}{1-m_2} \right) + P_2 \left( B_3r + \frac{B_6}{3}r^3 \right)
\]

Also, for the Fixed-Free boundary condition, the following components are changed as:
\( X_{11} = a^{m_1}, X_{12} = a^{m_2}, X_{13} = B_8, X_{14} = B_7, X_{15} = X_{16} = 0 \)
\( X_{21} = b^{m_1}, X_{22} = b^{m_2}, X_{23} = B_8, X_{24} = B_7, X_{25} = X_{26} = 0 \)  
(A.6)

\[
S_1 = B_3 r + B_8 r^3 - \frac{B_3 r}{(1-m_1)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_1} \right) + \frac{B_3 r}{(1-m_2)(m_2-m_1)} \left( \ln(r) - \frac{1}{1-m_2} \right)
\]  
(A.7)

Besides, for the state of creep progress, the components of \( X \) are as before case and the component of \( E \) for Free-Free boundary condition can be rewritten as:

\[
H \begin{bmatrix} D_1 & D_2 & \hat{A}_1 & \hat{A}_2 & J_1 & J_2 \end{bmatrix}^\top = E ,
\]  
(A.8)

\[
E = \begin{bmatrix} S_1(a) \\ S_1(b) \\ S_2(a) \\ S_2(b) \\ S_3(a) \\ S_3(b) \end{bmatrix}
\]

\[
S_1 = C_1 \left( \frac{\partial G_{11}}{\partial r} r^{m_1} + G_{11} m_1 r^{m_1-1} + \frac{\partial G_{21}}{\partial r} r^{m_2} + G_{21} m_2 r^{m_2-1} \right) + C_2 r^{-1} \left( G_{11} r^{m_1} + G_{21} r^{m_2} \right) - b_0 r^{-1} \sigma^{m_1} \left( C_1 \left( \sigma_r - 0.5 \sigma_\theta \right) + C_2 \left( \sigma_\theta - 0.5 \sigma_r \right) \right)
\]  
(A.10)

\[
S_2 = \int \left( L_1 \left( \frac{\partial G_{11}}{\partial r} r^{m_1} + G_{11} m_1 r^{m_1-1} + \frac{\partial G_{21}}{\partial r} r^{m_2} + G_{21} m_2 r^{m_2-1} \right) + L_2 \left( G_{11} r^{m_1} + G_{21} r^{m_2} \right) \right) \left( \varepsilon_{\sigma r} - \varepsilon_{\sigma \theta} \right) dr
\]  
(A.11)

\[
S_3 = \int \left( P_1 \left( \frac{\partial G_{11}}{\partial r} r^{m_1} + G_{11} m_1 r^{m_1-1} + \frac{\partial G_{21}}{\partial r} r^{m_2} + G_{21} m_2 r^{m_2-1} \right) + P_2 \left( G_{11} r^{m_1} + G_{21} r^{m_2} \right) \right) \left( \varepsilon_{\sigma r} - \varepsilon_{\sigma \theta} \right) dr
\]  
(A.12)

Also, for the Fixed-Free boundary condition, the following components are changed as:
\[ S_1 = G_1 r_1^{m_1} + G_2 r_2^{m_2} \]  \hspace{1cm} (A.13)

**Nomenclature**

- \( a \): Inner radius of disc
- \( b \): Outer radius of disc
- \( B_r \): Magnetic induction [T]
- \( C_{ij0} \): Temperature and moisture independent elastic coefficient [N/m\(^2\)]
- \( c_{ij} \): Elastic coefficient [N/m\(^2\)]
- \( D_t \): Electric displacement [C/m\(^2\)]
- \( d_{11} \): Magnetic coefficient [Ns\(^2\)/C\(^2\)]
- \( e_{1j} \): Piezoelectric coefficient [C/m\(^2\)]
- \( k^C \): Moisture diffusivity coefficient
- \( k^T \): Thermal conductivity coefficient
- \( m_1 \): Pyromagnetic coefficient [N/AmK]
- \( p_1 \): Pyroelectric coefficient [C/m\(^2\)K]
- \( q_{1j} \): Piezomagnetic coefficient [N/Am]
- \( \chi_1 \): Hygroelectric coefficient [Cm/kg]

**Greek symbols**

- \( \alpha_i \): Thermal expansion coefficient [1/K]
- \( \alpha^* \): Empirical material coefficients for moisture dependence
- \( \beta \): Inhomogeneity parameter
- \( \beta_i \): Moisture expansion coefficient [m\(^3\)/kg]
- \( \beta^* \): Empirical material coefficients for temperature dependence
- \( \beta_{11} \): Dielectric coefficient [C\(^2\)/Nm\(^2\)]
- \( \gamma_1 \): Hygromagnetic coefficient [Nm\(^2\)/Akg]
\( \varepsilon_{11} \) electromagnetic coefficient [Ns/VC]

\( \lambda \) thermal modulus [N/m²K]

\( \zeta \) hygroscopic stress coefficient

\( \rho \) Density [kg/m³]

\( \sigma_i \) Stress [N/m²]

\( \phi \) electric potential [W/A]

\( \psi \) magnetic potential [A]

\( \omega \) rotating speed [rev/min]

References


