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Multi-objective Optimization of Surface Roughness and Material Removal Rate Using an Improved Self-Adaptive Particle Swarm Optimization Algorithm in the Milling process

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ABSTRACT: Surface roughness is one of the main characteristics of a work piece in the quality control process. Several parameters such as cutting tool material and geometry, cutting parameters, work piece material properties, machine tool and coolant type affect the surface quality. An important task of process planners is the proper selection of three main cutting parameters: cutting speed, feed rate, and depth of cut in order to have not only low surface roughness, but also to perform the process within a reasonable amount of time. In this paper, using full factorial experiment design, the multiple regression equation for the surface roughness in the climb milling process of DIN 1.4021 martensitic stainless steel has been obtained and then used as one of the objective functions in the Multi-objective Improved Self-Adaptive Particle Swarm Optimization (MISAPSO) algorithm. This algorithm has been used to obtain cutting parameters to achieve low surface roughness simultaneously with a high material removal rate. The relatively new algorithm MISAPSO developed with some changes in the common particle swarm optimization (PSO) technique, has been used in multi-objective optimization of machining processes and was shown to be able to help the process planners in selecting cutting parameters.

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1- Introduction

Global steel consumption is progressively increasing. In the manufacturing process of a large percentage of parts made of steel, conventional chip removal operations, including milling are used. Martensitic stainless steels, like DIN 1.4021, are widely used in applications for which a combination of high strength and good corrosion resistance is needed such as shear blades and surgical equipment. One of the main challenges that the process planner faces to achieve a high quality work piece is the proper selection of cutting parameters. One of the most important factors in the final quality control of a piece is to consider its surface finish. The surface roughness has a great influence on the corrosion resistance and tribological properties of the piece. For this reason, the proper selection of cutting conditions i.e. cutting speed, feed rate and depth of cut is of great significance and remains as an important topic in manufacturing engineering.

Benardos and Vasniakos [1] carried out a comprehensive literature review of the prediction models for surface roughness. They said that the cutting theory-based models are not exact. This is because of that the mechanisms leading to the formation of surface roughness are very complicated and interacting with nature. Due to the nonlinear and intricate relationship between machining outputs, such as cutting force, tool life and surface roughness, and the cutting parameters, models based on experimental data have been widely developed. These models can be classified into two major categories [2]: (i) models that examine the effects of input factors on the response by employing the multiple regression method and the analysis of variance to establish this relationship; and (ii) artificial intelligence (AI) based models.

Feng and Wang [3] developed a statistical model for the prediction of surface roughness using nonlinear regression method in turning process. Also, they investigated the effect of cutting parameters, tool point angle, cutting time and work piece hardness on the surface roughness. Ozcelik and Bayramoglu [4] presented an empirical model for the estimation of surface roughness in a high-speed milling operation. These researchers found that the first and second order models developed were in a good agreement with the real values.

Aouici et al. [5] determined the influence of cutting speed, feed rate and cutting time on the tool wear and the surface roughness in turning process of X38CrMoV5-1 steel with a CBN tool using ANOVA and the response surface method (RSM). The authors concluded that the feed rate was the most effective factor on the surface roughness. Asilturk and Cunkas [1] used an artificial neural network (ANN) and multiple regression method to analyze the effect of speed, feed, and depth of cut on the surface roughness of AISI 1040 steel. The predicted values were found to be close to the measured values for both developed models, and the feed rate was the dominant factor affecting the surface roughness followed by the depth of cut and cutting speed. Bharathi Raja and Baskar [6] developed a mathematical model for surface roughness prediction using Particle Swarm Optimization (PSO) on the basis of experimental results in the face milling of aluminum. They found that the predicted roughness using PSO technique was in a good agreement with the measured values.

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Kivak [7] applied the Taguchi method and regression analysis to evaluate the machinability of Hadfield steel with PVD and CVD coated inserts under dry milling condition. It was shown that the Taguchi method was very successful in the optimization of cutting parameters for having minimum surface roughness and flank wear. Acayaba and Escalona [8] used experimental data to develop predictive models using multiple linear regression (MLR) and ANN methods. They found that the ANNs were better than MLR for predicting surface roughness in turning processes. Moreover, the authors used the suggested ANN as the fitness function in Simulated Annealing (SA) optimization algorithm in order to obtain a group of cutting parameters that lead to a low surface roughness. Hanief and Wani [9] developed a mathematical model to characterize the surface roughness during the running-in wear process. They said that the ANN model can be used to predict the surface roughness with a high accuracy. Gok [10] presented a new approach to minimize the surface roughness and cutting force via multi-objective grey design and response surface analysis in turning of ductile iron. The study concluded that the depth of cut was the dominant property on the surface roughness and cutting forces. Gupta and Kumar [11] modeled the two response variables i.e. surface roughness and material removal rate (MRR) for turning of unidirectional glass fiber reinforced plastics (UD-GFRP) composite using Principal Component Analysis (PCA) and the Taguchi method. The optimum combination of cutting parameters was found for maximum MRR and minimum surface roughness. The obtained results were verified through confirmation experiments.

Particle swarm optimization algorithm has been used in various research fields such as aerodynamic optimization of a horizontal axis wind turbine blade [12] and updating boring bar's dynamic model [13], but the use of that to optimize the machining processes has been little done in relation to other fields of research. The aim of the present study is to investigate the effects of the cutting parameters i.e. cutting speed, feed rate, and radial depth of cut on the surface roughness and MRR in the milling process of DIN 1.4021 stainless steel. Using the multiple linear regression method an equation has been obtained for surface roughness, and this equation has been used as one of the objective functions in a multi-objective improved self-adaptive particle swarm optimization (MISAPSO) algorithm in order to achieve the cutting parameters that result in a low surface roughness and high material removal rate simultaneously. In this study, the power of the relatively new algorithm MISAPSO which was developed with some changes in the traditional particle swarm optimization method has been investigated in the optimization of cutting parameters. The performance and efficiency of this technique have not yet been studied in the published research works in the field of machining optimization. The process planners can use this procedure for selecting the proper cutting parameters in order to get a minimum surface roughness and maximum MRR.

2- Experimental Work

A cubic sample of DIN 1.4021 martensitic stainless steel was used to conduct the milling experiments without coolant. This steel has a chemical composition of 15%C, 1%Mn, 1%Si, 0.04%P, 0.03S and 12-14%Cr [14]. TiN-coated 4-flute flat end mills from HSS with a diameter of D=10 mm were

selected for this examination. Once each set of nine tests were carried out on an FP 4 MA CNC milling machine, the work piece was positioned in a bench and a Surtronic 3+ surface roughness measuring machine was used to measure the roughness of the work piece with a cut-off value of 0.8 mm. The surface roughness was measured in the feed direction of the work piece. Figure 1 shows the experimental setup and the surface roughness measuring machine. The specification of CNC milling machine and surface roughness measuring machine have been given in Table 1.

Table 1. Specification of CNC milling machine and surface roughness measuring machine

roughness m	roughness measuring machine					
Specification of CNC milling machine	Specification of the surface roughness measuring machine					
Make: DECKEL Maho	Make: Taylor Hobson					
Work table size: 480 mm × 800 mm	Resolution: 0.01 µm					
Spindle speed:	Stylus type:					
63 – 3150 rpm	112/1502: Diamond					
Feed: 2 – 3000 mm/min	Tip radius: 5 μm					



Fig. 1. Experimental setup and surface roughness measuring machine

The surface roughness average (R_a) was defined on the basis of the ISO 4287 norm [15] as the arithmetical mean of the deviations of the roughness profile from the central line along the measurement. This definition can be expressed as:

$$R_{a} = \frac{1}{l} \int_{0}^{l} |y(x)| dx \tag{1}$$

where y(x) is the coordinate of the roughness profile and *l* is the evaluation length.

To reduce the effect of noise parameters, the surface roughness was measured three times at different parts of the work piece and their average has been recorded. From the many effective parameters on the surface roughness in milling, the effect of three main cutting parameters, cutting speed (V), feed rate (f), and radial depth of cut (a_r) were investigated in this study. Levels of cutting parameters have been selected according to the tool, workpiece materials and the tool maker specifications presented in Table 2. Constant cutting conditions in the experiments include an axial cutting depth of $a_a = 5$ mm and the climb milling process. In climb milling, the cutting tool is fed with the direction of rotation. Figure 2 illustrates schematically the cutting parameters in the climb end milling process.

Table	2	Cutting	Conditions	in	Experimental	Tests
Table .	<i>-</i> .	Cutting	Conditions		Experimental	ICOLO

Cutting speed (m/min)	Feed rate (mm/rev)	Radial depth of cut (mm)
15	0.2	0.3
25	0.4	0.6
40	0.8	0.9



Fig. 2. The cutting parameters in climb end milling process

Table 3 shows the cutting parameters and the average surface roughness in each experiment. The full factorial experiment design was selected, and in total, 27 experiments were conducted. Each test was done once.

The material removal rate (MRR) in the end milling process is obtained from the following relationships [16]:

$$MRR = N f a_a a_r \tag{2}$$

where N is the spindle speed (rpm). By knowing the axial depth of cut $a_a=5$ mm and the relationship $V=\pi DN$, the material removal rate in mm³/s becomes:

$$MRR = 2.65V f a_r \tag{3}$$

This relationship for *MRR* and the obtained equation for surface roughness that can be found in the following section have been used as the objective functions in the optimization algorithm.

3- Results and Discussion

Based on the experimental data, the multiple linear regression was utilized to model the surface roughness. After ensuring the accuracy of the proposed regression equation, the Multi-objective Improved Self-Adaptive Particle Swarm Optimization (MISAPSO) algorithm was employed to

Fable 3	6. Exper	imental	parameters	and the	recorde	d average
		S	urface rough	ness		

surface roughness						
Test no.	V (m/min)	f (mm/rev)	<i>a</i> _{<i>r</i>} (mm)	$R_a(\mu m)$	<i>MRR</i> (mm ³ /s)	
1	15	0.2	0.3	1.37	2.39	
2	15	0.2	0.6	1.66	4.78	
3	15	0.2	0.9	1.76	7.17	
4	15	0.4	0.3	2.36	4.77	
5	15	0.4	0.6	1.96	9.54	
6	15	0.4	0.9	2.36	14.31	
7	15	0.8	0.3	2.73	9.54	
8	15	0.8	0.6	2.72	19.08	
9	15	0.8	0.9	1.99	28.62	
10	25	0.2	0.3	1.31	3.98	
11	25	0.2	0.6	0.87	7.95	
12	25	0.2	0.9	1.04	11.93	
13	25	0.4	0.3	2.11	7.95	
14	25	0.4	0.6	1.48	15.90	
15	25	0.4	0.9	1.34	23.85	
16	25	0.8	0.3	2.11	15.90	
17	25	0.8	0.6	1.60	31.80	
18	25	0.8	0.9	1.24	47.70	
19	40	0.2	0.3	1.52	6.36	
20	40	0.2	0.6	1.16	12.72	
21	40	0.2	0.9	1.07	19.08	
22	40	0.4	0.3	1.82	12.72	
23	40	0.4	0.6	0.65	25.44	
24	40	0.4	0.9	0.71	38.16	
25	40	0.8	0.3	2.69	25.44	
26	40	0.8	0.6	2.63	50.88	
27	40	0.8	0.9	2.92	76.32	

determine a set of optimum cutting parameters that minimize the surface roughness and maximize the material removal rate.

Analysis of variance (ANOVA) can be used to investigate the effect of one or several input parameters on an output parameter or response [17]. In this study, the analysis of variance with the aid of MINITAB software has been done to investigate the effects of input parameters and their interactions on the surface roughness. Table 4 presents the analysis of variance for the surface roughness. According to the performed analysis of variance in Table 3, the amounts of feed rate and cutting speed effect on surface roughness are 39.8% and 17.0%, respectively. The interaction of cutting speed and feed rate has 22.1% effect on the surface roughness.

3-1-Multiple linear regression

Multiple regression is a method that describes the statistical relationship between a response and two or more independent predictors. Regression often uses the method of least squares, which determines the equation for the straight line that minimizes the sum of the squared vertical distances between

Source	DF	Seq SS	Contr.	Adj MS	F	Р
a_r	2	0.882	7.77%	0.4408	4.59	0.047
f	2	4.517	39.83%	2.2586	23.51	0.000
V	2	1.927	16.99%	0.9635	10.03	0.007
$a_r \times f$	4	0.425	3.75%	0.1063	1.11	0.417
$V \times a_r$	4	0.320	2.82%	0.0798	0.83	0.542
$V \times f$	4	2.503	22.07%	0.6257	6.51	0.012
Error	8	0.769	6.78%	0.0961		
Total	26	11.096	100%			

Table 4. Analysis of variance for the surface roughness

the data points and the line [18]. Different adjustments were done using MINITAB 14 and the adjustment with the best coefficient of correlation was selected. The suggested regression equation with second-degree that takes into account the interactions of two factors is given by:

$$R_{a} = 4.70 - 0.2 W + 0.55f - 2.05a_{r}$$

+0.0032V² - 0.10f² + 1.85a_{r}² (4)
+0.0612V f - 0.0184V a_{r} - 0.73f a_{r}

The squared multiple correlation coefficient R^2 and the adjusted coefficient R^2adj of Eq. (4) is 0.714 and 0.563, respectively. R^2 is the percentage of the total variation in the response that is explained by input factors in the model. Adjusted R^2 is a useful tool for comparing linear models with different numbers of predictors. The adjusted R^2 increases only if the new predictor improves the model more than that which would be expected by chance.

The mean squared error (MSE) is a measure of how close a fitted line is to data points. The smaller the MSE, the closer the fit is to the data. If \hat{Y} is a vector of *n* predictions, and Y is the vector of observed values, then the MSE of the predictor can be estimated by:

$$MSE = \frac{1}{n} \sum_{i=1}^{n} (\hat{Y}_{i} - Y_{i})^{2}$$
(5)

The closer MSE is to 0, the better the proposed model. Here, the value of MSE=0.12 was achieved, which means a good approximation exists for empirical data. The analysis of variance showed that the feed rate (f) has the greatest effect on the surface roughness. The main effects plot is shown in Fig. 3.

3-2-Multi-objective optimization problem

The main aim of this paper is to find the optimum cutting parameters in order to simultaneously maximize the material removal rate and minimize the surface roughness in the milling process. Due to milling machine limitations and the cutting tool manufacturer suggestions, the values of cutting speed, feed rate, and radial depth of cut must be limited between their minimal and maximal experimental values. The multi-objective problem could be written as follows:



Fig. 3. Main effects plot for the mean of surface roughness

$$\begin{aligned} \text{Minimize } & R_a = F\left(V, f, a_r\right) \\ \text{Maximize } & MRR = G\left(V, f, a_r\right) \\ \text{Subject to } &: \begin{cases} V_{\min} \leq V \leq V_{\max} \\ f_{\min} \leq f \leq f_{\max} \\ a_{r_{\min}} \leq a_r \leq a_{r_{\max}} \end{cases} \end{aligned}$$
(6)

In the following, the Multi-objective Improved Self-Adaptive Particle Swarm Optimization (MISAPSO) algorithm is used to solve Eq. (6).

3-3-MISAPSO Algorithm

Due to the high speed of convergence and also not to settle at the point of local minimum, the PSO method is used in the solution of single-objective and also multi-objective optimization problems. The PSO is a repetitive algorithm that improves its position in each iteration according to the previous position and velocity of the particle, the best previous position of that particle, and the best position among the entire population. The position of the ith particle can be obtained from the following relation:

$$X_{i}^{(t+1)} = X_{i}^{(t)} + V_{i}^{(t+1)}$$
(7)

where t is the current iteration, and $X_i^{(j)}$ and $V_i^{(j)}$ are the position and velocity of the ith particle in the jth iteration, respectively. The velocity $V_i^{(t+1)}$ can be obtained as follows:

$$V_{i}^{(t+1)} = \omega V_{i}^{(t)} + c_{1}.rand_{1}(.).(P_{best_{i}}-X_{i}^{(t)}) + c_{2}.rand_{2}(.).(G_{best}-X_{i}^{(t)})$$
(8)

where ω is the inertia weight, c_1 and c_2 are learning factors, $rand_1(.)$ and $rand_2(.)$ are two random values between (0, 1), P_{best_1} is the best previous experience of the ith particle, and $G_{best_1}^{best_1}$ is the best experience among the entire population.

The inertia weight (ω) can be calculated from the following relation:

$$\omega = \omega_{max} - \frac{\omega_{max} - \omega_{min}}{Iter_{max}} \times Iter$$
(9)

where $\omega_{\rm max}$ and $\omega_{\rm min}$ are initial and final weights, respectively,

Itermax is the maximum iteration number and Iter is the current iteration number.

The MISAPSO algorithm has been used to overcome local optima problems in this study [19]. In MISAPSO, a chaotic improvement had been proposed to introduce a new inertia weight parameter, as seen below:

$$\omega_{new} = \omega \times c x_i^j \tag{10}$$

where cx_i^j is the jth chaotic variable and can be obtained from the following relationship [20]:

$$cx_{i} = \left[cx_{i}^{1}, cx_{i}^{2}, ..., cx_{i}^{n} \right]_{1 \times n}, i = 0, 1, 2, ..., N_{choas}$$

$$cx_{i+1}^{j} = 4 \times cx_{i}^{j} \times \left(1 - cx_{i}^{j} \right), j = 1, 2, ..., n$$

$$cx_{i}^{j} \in (0, 1), cx_{0}^{j} \notin \{ 0.25, 0.5, 0.75 \}$$

$$cx_{0}^{j} = rand (.)$$
(11)

where N_{choas} is the number of individuals, *n* is the number of surge arrester models parameters, and *rand*(.) is a random number in the range of (0, 1).

In traditional PSO, the learning factors c_1 and c_2 are considered constant, but in the MISAPSO algorithm, c_1 and c_2 are considered as two new factors which are added to the position vector. This means that in each iteration, the parameters c_1 and c_2 have been optimized too, as follows:

$$X = [Cutting \ parameters, c_1, c_2]$$
(12)

Usually, objective functions in a multi-objective optimization problem are in contradiction with each other. This means that there is no optimal solution for a multi-objective optimization problem, but instead, there is a set of optimal solutions called Pareto-optimal solutions.

A general multi-objective optimization problem could be written as follows [21]:

$$\begin{aligned} \text{Minimize} \quad & f_1(X), f_2(X), \dots, f_p(X) \\ \text{Subject to} : \begin{cases} g_i(X) < 0 & i = 1, 2, \dots, N_{eq} \\ h_i(X) = 0 & i = 1, 2, \dots, N_{ueq} \end{cases} \end{aligned} \tag{13}$$

where $f_i(X)$ is the ith objective function, $g_i(X)$ and $h_i(X)$ are the equality and inequality constraints, respectively; p is the number of objective functions, X is the vector of the optimization variables, and N_{eq} and N_{ueq} are the number of equality and inequality constraints, respectively.

If X_1 and X_2 are two solutions of a multi-objective optimization problem, two cases arise: one dominates the other or neither dominates the other. A solution X_1 dominates X_2 if the following two conditions are satisfied [19]:

$$\forall j \in \{1, 2, ..., p\}, f_{j}(X_{1}) \leq f_{j}(X_{2}) \exists k \in \{1, 2, ..., p\}, f_{k}(X_{1}) < f_{k}(X_{2})$$
(14)

If any of the two conditions in Eq. (14) is violated, X_1 does not dominate X_2 . The nondominated solutions in the entire search space form the Pareto-optimal solutions.

A fuzzy-based clustering procedure has been used to control

the size of the solution repository (for more details, see [19]). Figure 4 shows the MISAPSO algorithm has been used to solve the proposed multi-objective problem in Eq. (6).



Fig. 4. The MISAPSO algorithm flow chart

3- 4- Optimum cutting parameters

To show the implementation of the proposed algorithm, the case study introduced in section 2 has been considered. The MISAPSO algorithm has been used to find optimal cutting parameters which maximize the material removal rate and minimize the surface roughness, simultaneously. Table 5

Parameter	$V_{_{min}}$	V _{max}	f_{min}	f_{max}	a _{r,min}	a _{r,max}
Value	15	40	0.2	0.8	0.3	0.9

shows the limitations of the input parameters.

The Monte Carlo simulation has been used to show the feasibility space of solution [22]. The main goal of the MISAPSO algorithm is to find the optimal Pareto set of the feasibility space of solution. Figure 5 shows the feasibility space of the foregoing optimization problem. The results obtained from the MISAPSO algorithm are shown in Figure 6.



Fig. 5. The feasibility space of the optimization problem



Fig. 6. The Pareto-optimal set obtained from the MISAPSO algorithm

The obtained results depicted in Fig. 6 show that there is no optimum solution for Eq. (6). There is a set of optimal solutions (Pareto solutions). When the surface roughness of the work piece decreases, the material removal rate decreases, as well. Some Pareto-optimal cutting parameters obtained from the MISAPSO are shown in Table 6.

When a process planner must choose a proper solution from among all others, his/her skills and experiences will help him/her to make the right choice. The proposed algorithm is able to help the process planner in selecting the optimum

 Table 6. Some Pareto-optimal Solutions for the Multi-objective

 Optimization Problem of this Study

V (m/min)	f (mm/rev)	<i>a_r</i> (mm)	<i>R</i> _a (μm)	MRR (mm ³ /s)
34.4	0.31	0.86	0.94	23.9
33.5	0.32	0.84	0.95	24.2
36.2	0.49	0.90	1.36	41.4
34.5	0.54	0.84	1.38	42.3
32.4	0.59	0.88	1.44	44.5
30.0	0.71	0.87	1.61	49.4
28.8	0.76	0.86	1.68	49.9
31.7	0.74	0.90	1.69	56.0
38.8	0.79	0.88	2.11	71.4

cutting parameters to achieve low surface roughness and high material removal rate, simultaneously.

4- Conclusions

In the present study, using a full factorial experiment design, the effects of the cutting parameters i.e. cutting speed, feed rate, and radial depth of cut on the surface roughness in the climb milling process of stainless steel have been investigated. The main conclusions obtained from this study are as follows:

- 1. The feed rate was the most effective parameter on the surface roughness. With the aid of experimental results, the multiple linear regression equation for the surface roughness has been obtained. The value of Mean Squared Error for this regression equation was 0.12 which shows a good approximation.
- 2. The obtained regression equation and the material removal rate (*MRR*) formula have been used as the objective functions in a Multi-objective Improved Self-Adaptive Particle Swarm Optimization (MISAPSO) algorithm. Consequently, the optimum cutting parameters in order to minimize the surface roughness and simultaneously maximize the *MRR* have been achieved.
- 3. In multi-objective optimization problems, a set of optimal solutions exists called the Pareto-optimal solutions. In this paper, the relatively new algorithm MISAPSO derived from PSO method has been employed to find the Pareto-optimal solutions in a cutting process and its ability for optimization has been confirmed. The performance and efficiency of MISAPSO algorithm have not yet been studied in the literature reviews of the field of machining optimization.
- 4. Each of the optimal points proposed by the algorithm MISAPSO corresponds to the values of three parameters cutting speed, feed rate and radial depth of cut which optimize the material removal rate and surface roughness simultaneously. In other words, for an expected amount of surface roughness, the maximum allowable material removal rate with the values of corresponding cutting parameters was recommended by this optimization algorithm.

The proposed procedure can help the process planners in selecting optimum cutting parameters in order to simultaneously reach a low surface roughness and a high *MRR*.

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